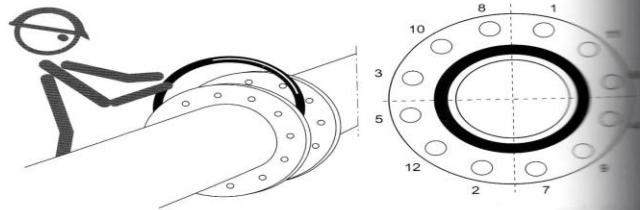


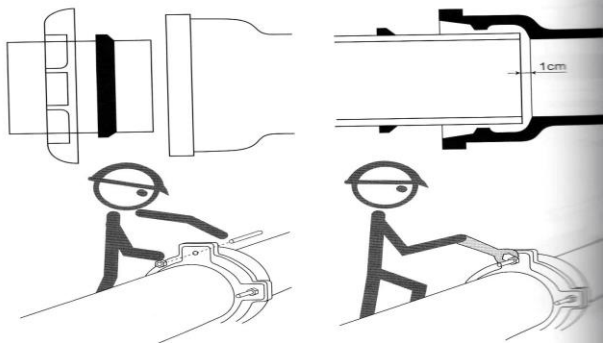
Water Supply Network



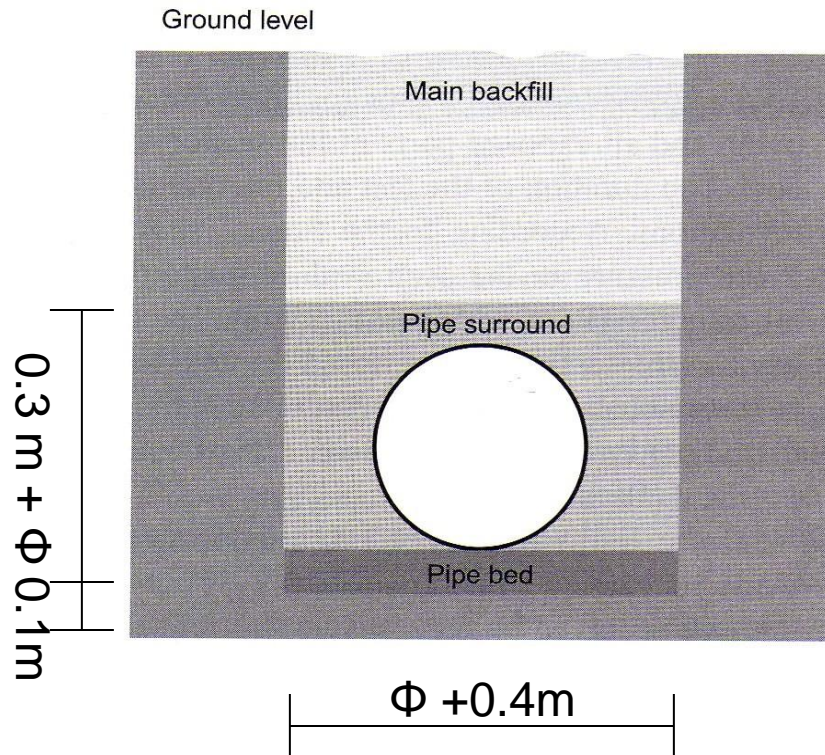
Flanged joints



Gland joints



Installation of water pipe

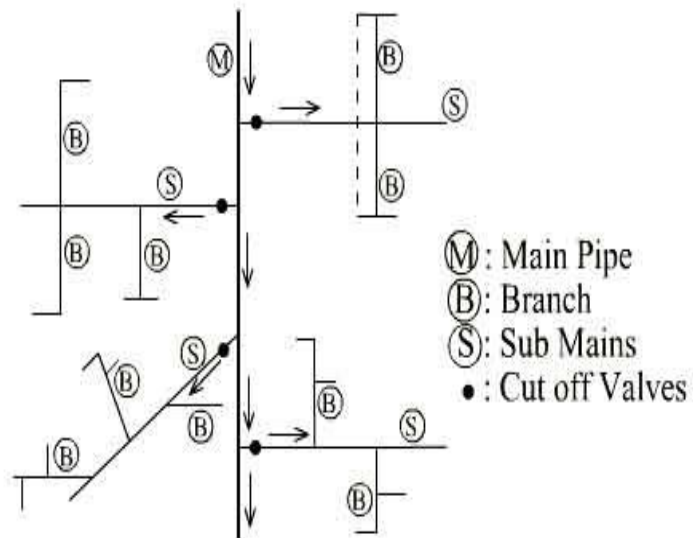


Planning of water distribution systems

Tree system (dead end system)

It is suitable for old towns and cities having no definite pattern of roads.

Dead End or Tree System



Advantages:

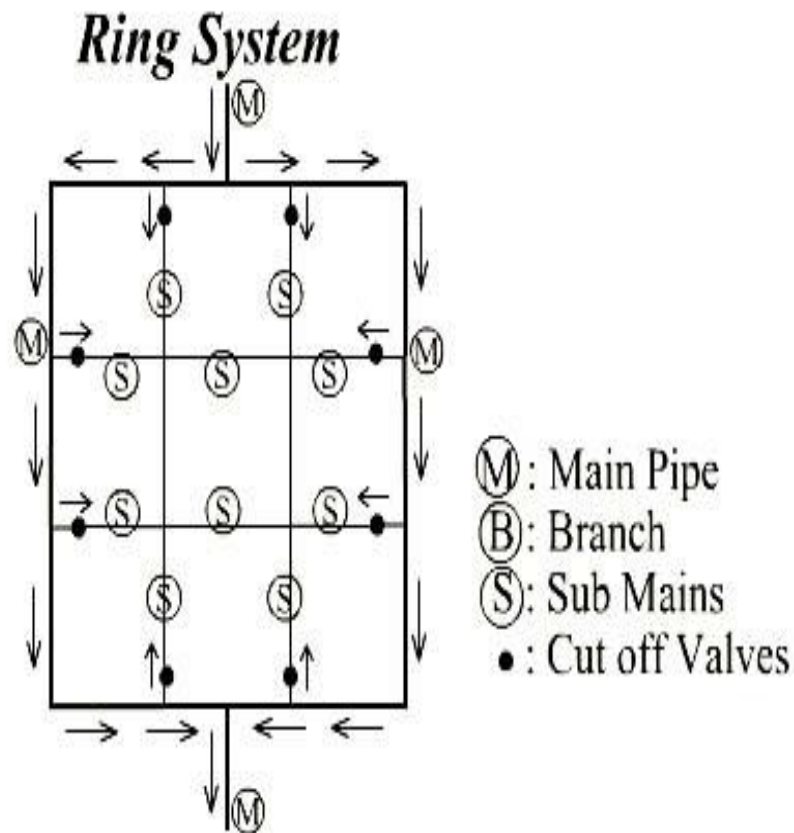
- Simple in design and construction.
- Low cost.

Disadvantages:

- Dead ends tend to reduce the pressure and pollute water.
- There are not enough valves to control the network.
- Difficulties in extension of the network.

Loop (Ring) system

The supply main is laid all along the peripheral roads and sub mains branch out from the mains.



Advantages:

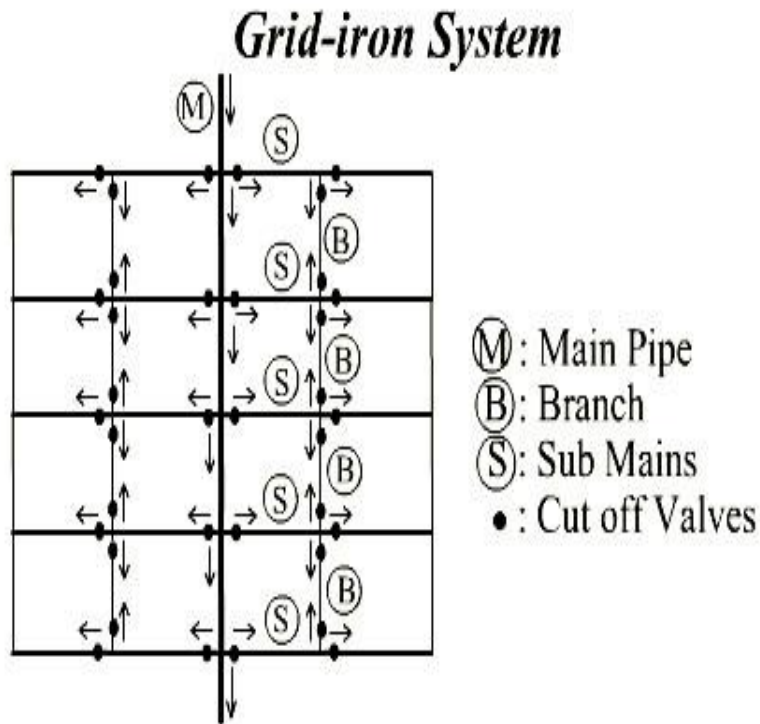
- Reduce the dead ends.
- There are valves on the lateral pipes to control the network.
- It is easy to extend the network.
- The water can reach every point in two directions.

Disadvantages:

- There are some of dead ends.

Grid iron system

It is suitable for cities with rectangular layout, where the water mains and branches are laid in rectangles.



Advantages:

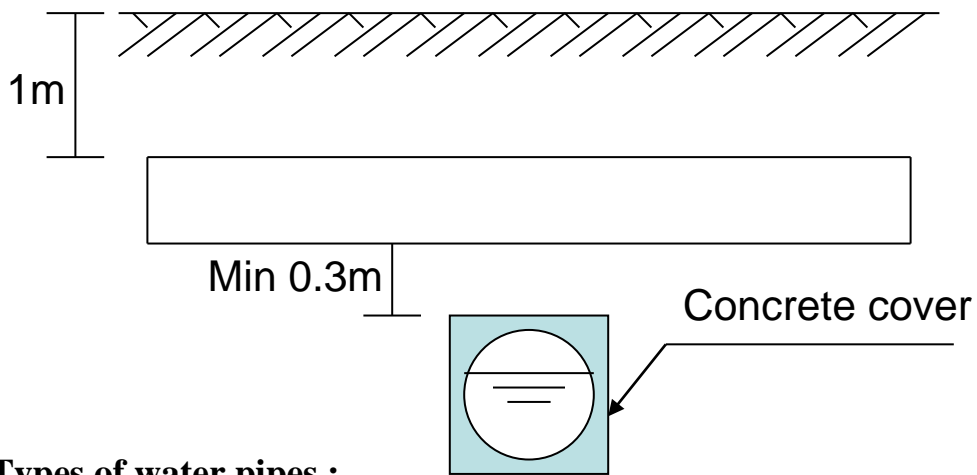
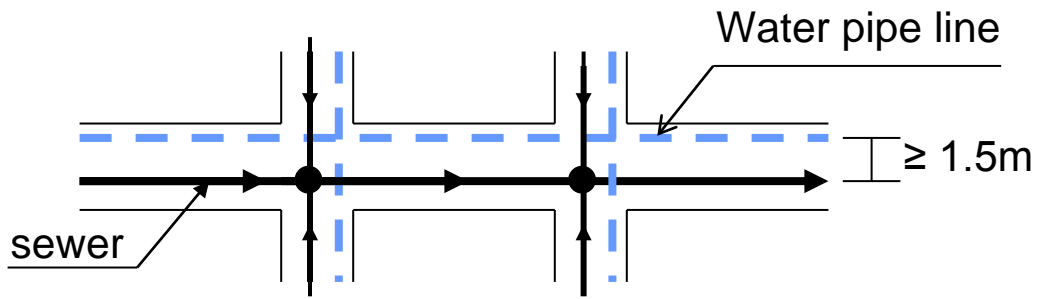
- Reduction in dead ends tends to improve the pressure.
- There are valves on the lateral pipes to control the network.
- It is easy to extend the network.
- The water can reach every point in two directions.

Disadvantages:

- There are some of dead end

| Comparison elements | Tree system | Loop system | Grid iron system |
|---|--------------------|--------------------|-------------------------|
| Cost | Minimum | Moderate | High |
| Dead ends | Many | Moderate | None |
| The range of damages due to broken pipe | Huge | Moderate | Limited |
| Water quality | Poor | Moderate | High |
| Water pressure at the ends | Low | Moderate | High |

Crossing of pipe line and sewer



Types of water pipes :

- Cast iron
- Ductile cast iron
- Steel
- Plastic pipes (e.g. UPVC).

| pipes type | Diameter (mm) |
|-----------------------------|---------------|
| U.P.V.C | 200 – 700 |
| Polly ethylene high density | 200 – 700 |
| G.R.P | 200 – 2800 |
| Ductile cast iron | 200 – 900 |
| Pre-stressed concrete | 600 – 3000 |

Design Criteria of pipes networks

- 1- The minimum diameter of pipe = 150 mm.
- 2- The velocity = 0.8 – 1.5 m/s.
- 3- The hydraulic gradient (S) = 1 ‰ - 3 ‰.
- 4- The pressure at the farthest and highest point in the network ≥ 25 m.
- 5- The valves ≤ 300 mm installed directly on the pipe line.
- 6- The valves ≥ 300 mm installed in valves room.
- 7- The design discharge
 - For transmission main
 $Q_d = Q_{\text{max daily}} + Q_f$
 - For main and secondary line
 $Q_d = Q_{\text{max daily}} + Q_f$ or $Q_{\text{max hourly}}$
 - For minor distribution
 $Q_d = Q_f$
 - For service connection
 $Q_d = Q_{\text{max hourly}}$

Fire demands

| Population (capita) | Q_f (l/s) |
|---------------------|-------------|
| 10,000 | 20 |
| 25,000 | 25 |
| 50,000 | 30 |
| 100,000 | 40 |
| More than 200,000 | 50 |

Design of water network

- Equivalent pipes method.
- Method of sections
- Method of circles.
- Hardy cross method.

Equivalent pipe method

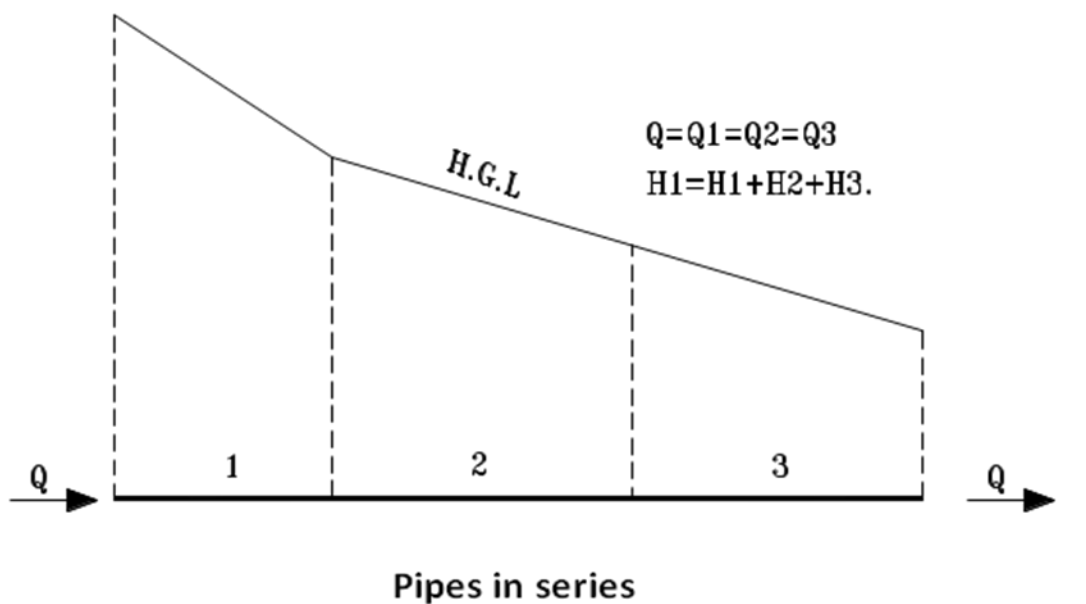
Equivalent pipe is a method of reducing a combination of pipes into a simple pipe system for easier analysis of a pipe network, such as a water distribution system.

An equivalent pipe is an imaginary pipe in which the head loss and discharge are equivalent to the head loss and discharge for the real pipe system. There are three main properties of a pipe: diameter, length, and roughness. As the coefficient of roughness, C , decreases the roughness of the pipe decreases. For example, a new smooth pipe has a roughness factor of $C = 140$, while a rough pipe is usually at $C = 100$. To determine an equivalent pipe, you must assume any of the above two properties. Therefore, for a system of pipes with different diameters, lengths, and roughness factors, you could assume a specific roughness factor (most commonly $C = 100$).

The most common formula for computing equivalent pipe is the Hazen-Williams formula.

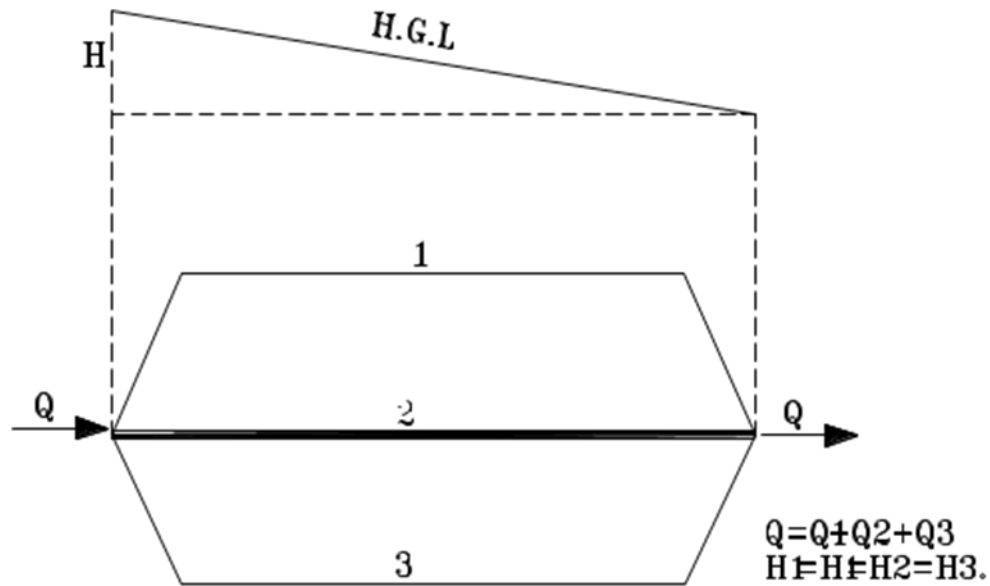
For example, pipes of different sizes connected in series can be replaced by an equivalent pipe of one diameter as follows:

Assume a quantity of discharge and determine the head loss in each section of the line for this flow, then using the sum of the sectional head losses and the assumed discharge, enter the chart to find the equivalent pipe diameter.



For pipe systems connected in parallel, a head loss is assumed, and the quantity of discharge through each of the pipes is calculated for that head

loss. Then the sum of the discharges and the assumed head loss are used to determine the equivalent pipe diameter.



Pipes in parallel

Hydraulic design of water network

The equations used in the design of water network:

1- $Q = A \times v$ discharge equation

2- $hf = \frac{flv^2}{2gd}$ Darcy - weisbach equation

3- $v = 0.355 \times C \times R^{0.63} \times S^{0.54}$ Hazen William equation

$$R = \frac{A}{p} = \frac{d}{4}$$

$$Q = 0.278 \times C \times D^{2.63} \times S^{0.54}$$

Hazen William monograph

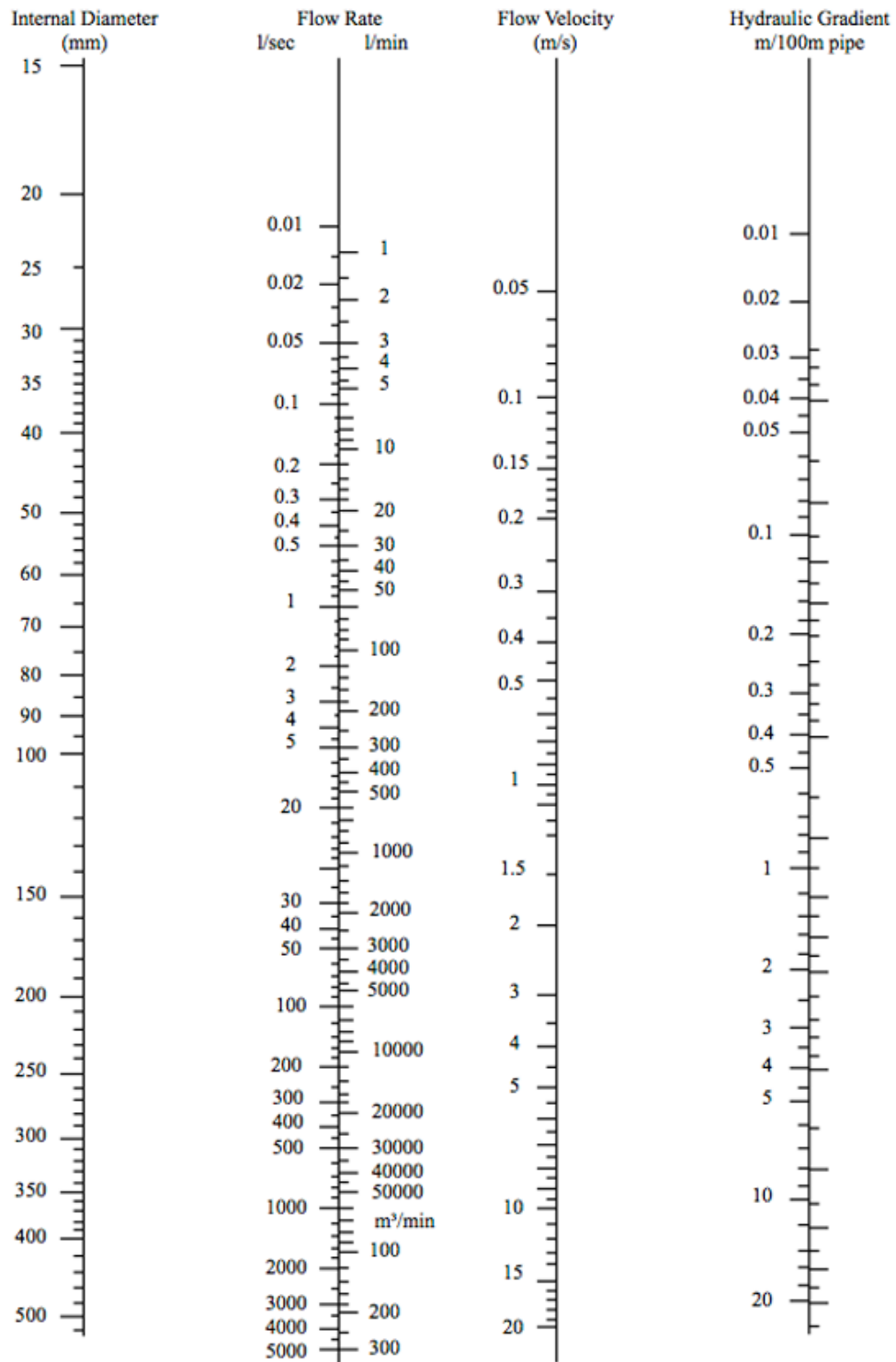
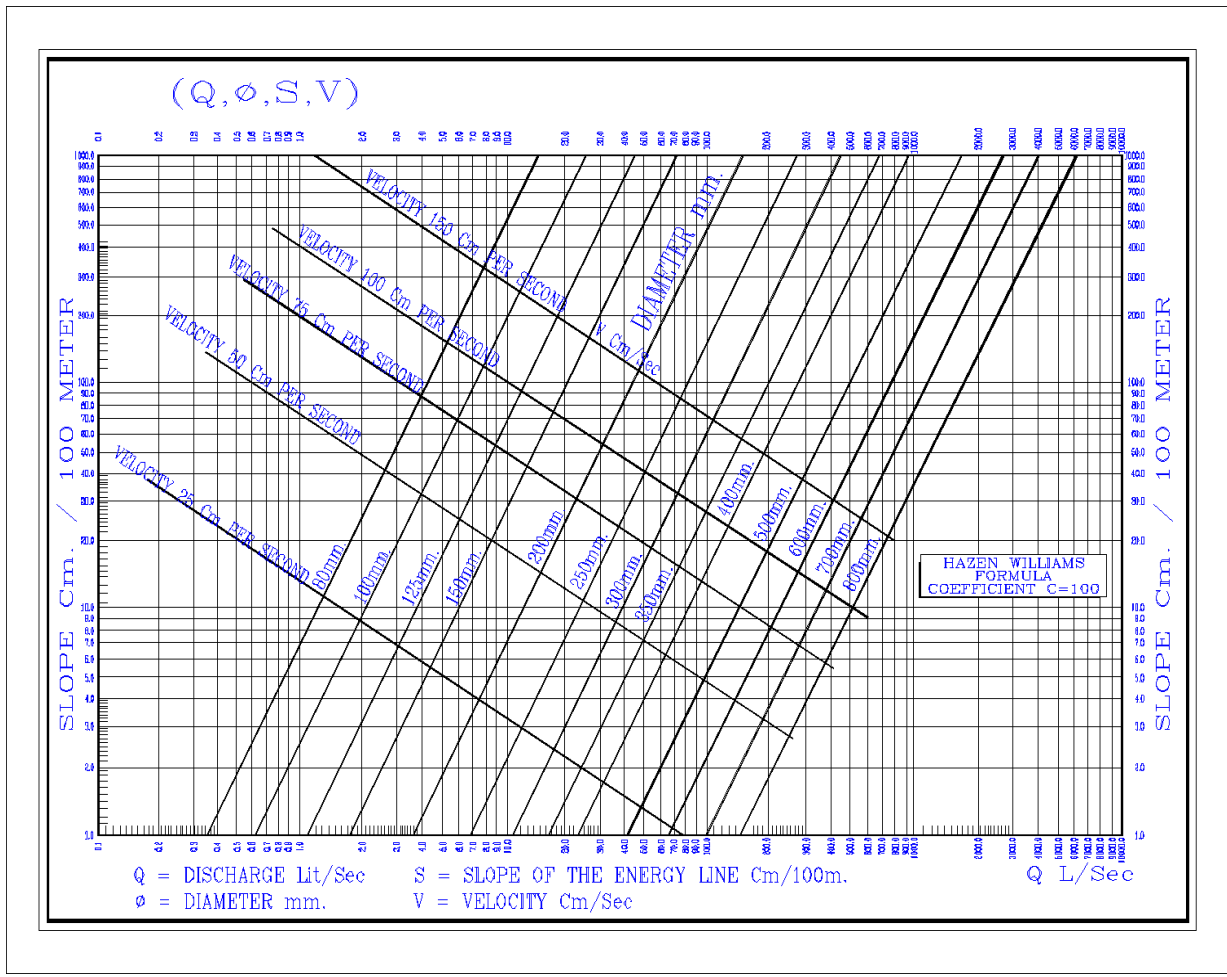


Diagram for water at 20 °C

Approximate values only



Example 1:

If a 400 mm water main (C =100) is discharging a flow of 150 lit/ sec, what is the velocity of flow and head loss?

Solution:

$Q = 150 \text{ lit/ sec} = 0.15 \text{ m}^3/\text{sec}$

$D = 400 \text{ mm} = 0.40 \text{ m}$

- Using (Hazen – Williams formula)

$Q = 0.278 C D^{2.63} S^{0.54}$

$S^{0.54} = \frac{0.15}{0.278 \times 100 \times (0.4)^{2.63}} = 0.060065$

$S = 0.00547 \text{ m/m} = 5.47 \text{ m/1000m}$

- Using the Hazen Williams monograph

$Q = 150 \text{ lit/sec} \ \& \ D = 400\text{mm}$

We get $V = 1.19$

$S = 5.45 \text{ m/ 1000 m}$

Example 2:

Design the main water supply pipe line for a city of population 30000 capita and average annual water consumption 200 l/c/d, consider required fire flow is 30 lit/sec.

Solution:

$$Q_{av} = \text{pop} \times q_{av} / 24 \times 60 \times 60 \\ = 30,000 \times 200 / 24 \times 60 \times 60 = 69.44 \text{ l/s}$$

$$Q_{\text{max daily}} = 1.8 \times Q_{av} \\ = 1.8 \times 69.44 = 125 \text{ l/s}$$

$$Q_{\text{max daily}} + Q_f = 125 + 30 = 155 \text{ l/s}$$

$$Q_{\text{max hourly}} = 2.5 \times Q_{av} \\ = 2.5 \times 69.44 = 173.61 \text{ l/s}$$

$$Q_d = 173.61 \text{ l/s}$$

Assume $S = 2 \text{ ‰}$, $Q_d = 173.61 \text{ l/s}$ from Hazen Williams monograph

We get $D = 520 \text{ mm} \approx 500 \text{ mm}$ $V = 0.83 \text{ m/sec}$

Example of pipes of different sizes connected in series

Find the equivalent pipe.

1- Assume $Q = 100 \text{ l/s}$

2- For the pipe AB from the monograph ($Q=100 \text{ l/s}$, $\phi= 350\text{mm}$) get $S = 4.5 \text{ ‰}$

$$S = hf / L$$

$$4.5 / 1000 = hf_{AB} / 1000 \quad \text{Then } hf_{AB} = 4.5 \text{ m}$$

For the pipe BC from the monograph ($Q=100 \text{ l/s}$, $\phi= 250\text{mm}$) get $S = 24 \text{ ‰}$

$$S = hf / L$$

$$24 / 1000 = hf_{BC} / 800 \quad \text{Then } hf_{BC} = 19.2 \text{ m}$$

Total head loss $h_T = hf_{AB} + hf_{BC}$

$$h_T = 4.5 + 19.2 = 23.7 \text{ m}$$

4- Assume $\phi = 300 \text{ mm}$

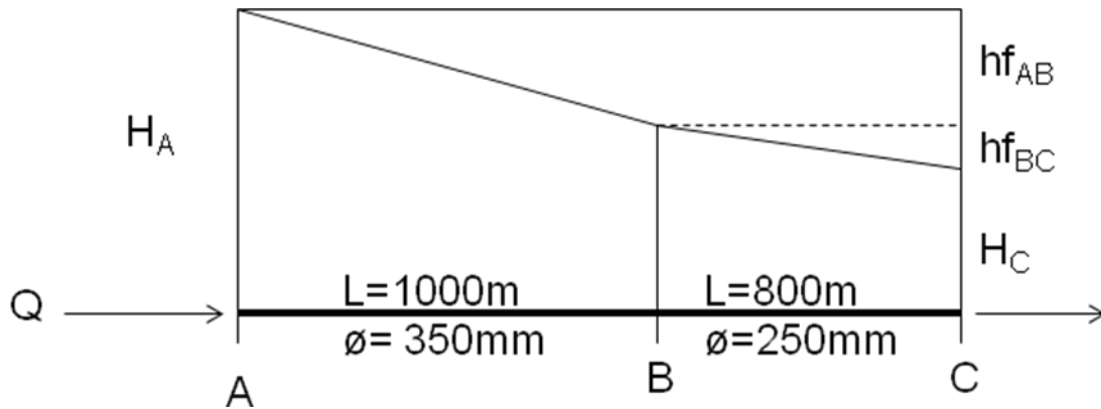
From the monograph

($Q=100 \text{ l/s}$, $\phi= 300\text{mm}$)

get $S_e = 9.5 \text{ ‰}$

$$S_e / 1000 = h_T / L_e$$

$$L_e = 23.7 \times 1000 / 9.5 \\ = 2495.74 \text{ m}$$



Example of pipes of different sizes connected in parallel

Find the equivalent pipe.

1- The head loss in the parallel pipes are equal assume $hf = 10 \text{ m}$

$$Q_T = Q_1 + Q_2$$

2- For the track ABCD: $hf_1=10\text{m}$, $L_1=1000\text{m}$, $\varnothing_1 = 250 \text{ mm}$

$$S_1 = hf_1 / L_1$$

$$S_1 = 10 / 1000 = 10 \text{ ‰}$$

From the monograph ($S_1= 10 \text{ ‰}$, $\varnothing_1 = 250 \text{ mm}$) get $Q_1 = 65 \text{ l/s}$

For the track AFED: $hf_2=10\text{m}$, $L_2=1000\text{m}$, $\varnothing_2 = 300 \text{ mm}$

$$S_2 = hf_2 / L_2$$

$$S_2 = 10 / 1000 = 10 \text{ ‰}$$

From the monograph ($S_2 = 10 \text{ ‰}$, $\varnothing_2 = 300 \text{ mm}$) get $Q_2 = 105 \text{ l/s}$

3- The discharge of the equivalent pipe

$$Q_T = Q_1 + Q_2$$

$$= 65 + 105 = 170 \text{ l/s}$$

Assume $\varnothing_e = 300 \text{ mm}$

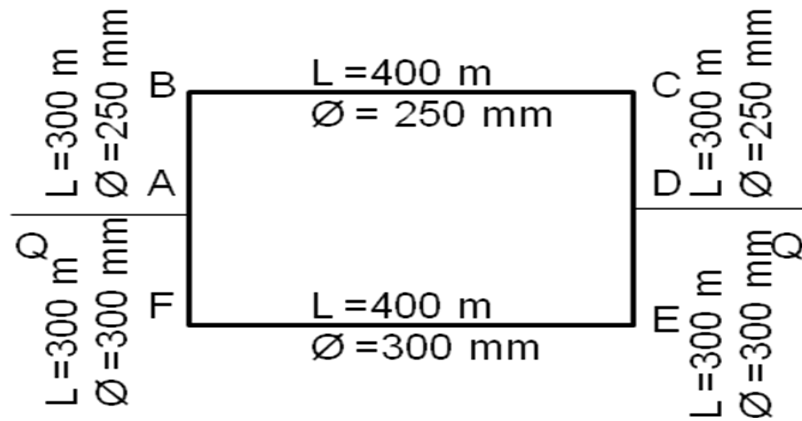
From the monograph ($Q_T = 170 \text{ l/s}$

, $\varnothing_e = 300 \text{ mm}$) get $S_e = 26 \text{ ‰}$

$$S_e = hf_T / L_e$$

$$L_e = 10 \times 1000 / 26$$

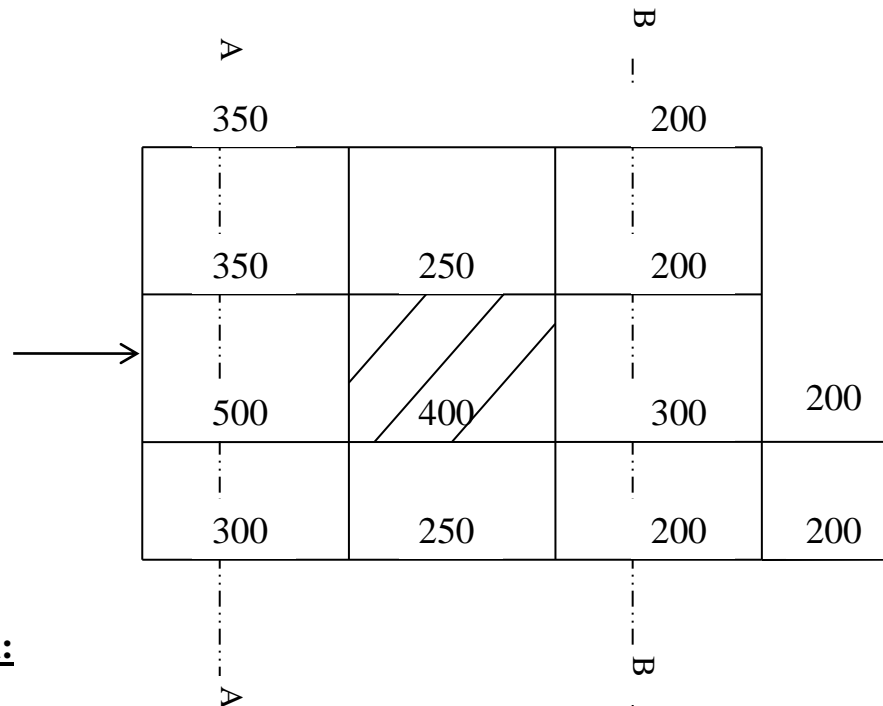
$$L_e = 384.62 \text{ m}$$



Method of sections

Example:

- The population served by Section A – A is 70 % of the population.
- The population served by Section B – B is 20 % of the population.
- Population = 100,000 capita.
- Average water consumption = 200 l/c/d.



Solution:

Section A – A:

Population = 0.7 x 100,000 = 70,000 capita

$Q_{av} = \text{pop} \times q_{av} / 24 \times 60 \times 60$

$= 70,000 \times 200 / 24 \times 60 \times 60 = 162 \text{ l/s}$

$Q_{\text{max daily}} = 1.8 \times Q_{av}$

$$= 1.8 \times 162 = 291.67 \text{ l/s}$$

$$Q_{\text{max daily}} + Q_f = 291.67 + 40 = 331.67 \text{ l/s}$$

$$Q_{\text{max hourly}} = 2.5 \times Q_{\text{av}}$$

$$= 2.5 \times 162 = 405 \text{ l/s}$$

$$Q_d = 405 \text{ l/s}$$

Number of pipes cut by section A – A:

2 ϕ 350 , 1 ϕ 500 , 1 ϕ 300

Assume S = 20 cm / 100 m.

$$Q_{\text{act}} = 2 \times 85 + 210 + 55 = 435 \text{ l/s}$$

Chick:

$$Q_{\text{act}} - Q_d / Q_d \times 100 = 435 - 405 / 405 \times 100 = 7.4 \%$$

$\pm 10 \%$ ok

Section B – B:

$$\text{Population} = 0.2 \times 100,000 = 20,000 \text{ capita}$$

$$Q_{\text{av}} = \text{pop} \times q_{\text{av}} / 24 \times 60 \times 60$$

$$= 20,000 \times 200 / 24 \times 60 \times 60 = 46.3 \text{ l/s}$$

$$Q_{\text{max daily}} = 1.8 \times Q_{\text{av}}$$

$$= 1.8 \times 46.3 = 83.34 \text{ l/s}$$

$$Q_{\text{max daily}} + Q_f = 83.34 + 25 = 108.34 \text{ l/s}$$

$$Q_{\text{max hourly}} = 2.5 \times Q_{\text{av}}$$

$$= 2.5 \times 46.3 = 115.75 \text{ l/s}$$

$$Q_d = 115.75 \text{ l/s}$$

Number of pipes cut by section B – B:

3 ϕ 200 , 1 ϕ 300

Assume S = 20 cm / 100 m.

$$Q_{\text{act}} = 3 \times 18 + 55 = 109 \text{ l/s}$$

Chick:

$$Q_{\text{act}} - Q_d / Q_d \times 100 = 109 - 115.75 / 115.75 \times 100 = - 5.83 \%$$

$\pm 10 \%$ ok